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Precise Interferometric Phase Determination

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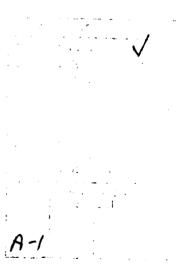
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PRECISE INTERFEROMETRIC PHASE DETERMINATION

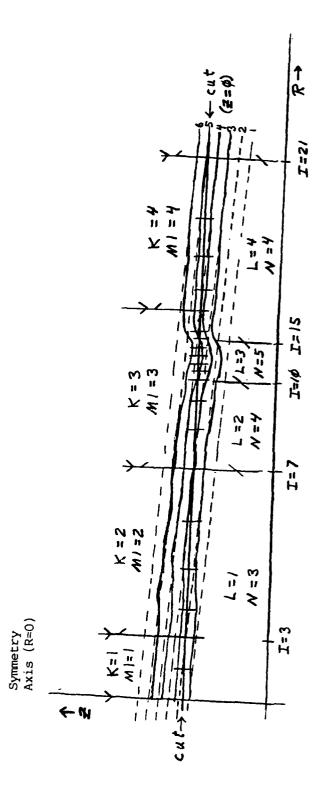
I. INTRODUCTION

This report is primarily concerned with precise phase-shift determinations where the phase changes rapidly (steep-gradient region) or where the phase changes are small (outer, low-density region). The medium is assumed to have cylindrical symmetry. Two things are required: A precise knowledge of the initial phase (from a pre-shot interferogram) and a precise determination of the final phase by interpolating the shifted fringes of the data interferogram. Abel inversion of the phase-shift information may reveal important low-density structures which would be missed without using these techniques. One should note, in the Abel inversion procedure, that the density determination at a particular cylindrical radius does not depend on what happens at smaller radii. Non-uniform fringe spacing may be important in the steep-gradient regions and is included in the interpolation procedure.

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The purpose of this report is to provide a general background and to set forth the method in a step-by-step procedure that can be put to practical use. The book-keeping details turned out to be rather involved and tricky. Thus, it seemed reasonable to include a detailed procedure for obtaining the necessary input from the pair of pre-shot and data interferograms as well as a listing of the computer program. The procedure is applied to a sample interferogram pair (Fig. (1)) obtained from a laser-produced plasma. The procedure includes preparing the interferogram pair for data extraction, tabulation of the data, and input to the computer program. The computed results (radius and phase shift) are given for the sample interferogram pair. I have attempted to make the program readable by the liberal use of comments to explain and de-limit.

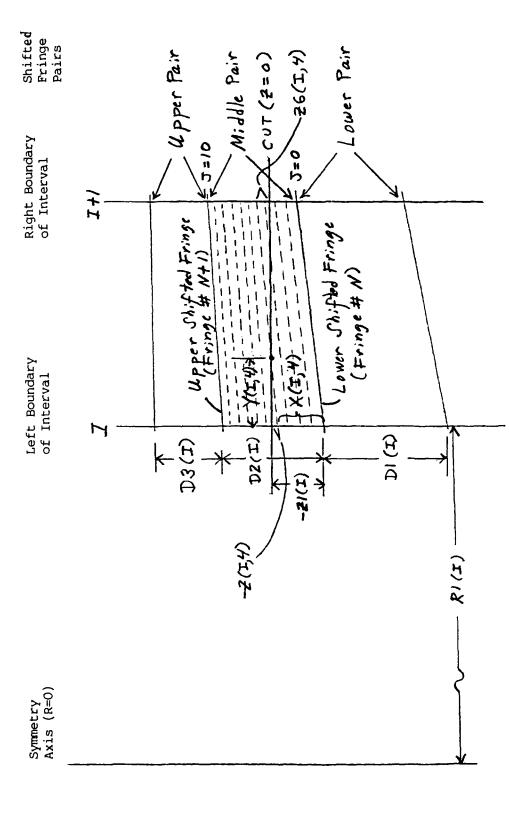
The example illustrated in Fig. 1 is an experimentallyobtained interferogram pair from a plasma containing a laserproduced blast, wave (I_9 to 16). The method to be described
provides useful phase-shift information for the region of the
blast wave and the outer-most, low density region (I>16).
However, the central region (I<7) shows such irregular phase
variation that the method offers no advantage in that region.



Sample interferogram pair with 6 initial, or unshifted (dashed) and 4 shifted (continuous curves) fringes bounding the cut, showing intervals (I), spans (K), and crossing regions (L, between lower shifted fringe crossings). Also shown are the lower unshifted (MI) and shifted (N) fringe numbers and the boundaries of intervals (+ cut), spans (\tau), unshifted fringe crossings (\tau) and shifted Fig. 1

II. BASIC METHOD

We wish to determine the radial density profile at a given axial postion Z, which is represented by the line Z = constant (called the "cut") in the R-Z plane of the interferogram pair. See Fig. 1. The final (shifted) fringes in the region of the cut are first divided into a sufficiently large number of radial "intervals" that the fringes are linear in each interval. Next, the region within the interval and between the two fringes bounding the cut is divided into 10 regions by introducing decimal "fringelets" which may be spaced non-uniformly to accomodate information in differing adjacent fringe spacings. The fringelets are illustrated in Fig. 2 with dashed lines but, in practice, are only treated numerically with the computer program. The non-uniform interpolation or fringelet spacing is described in the appendix. Each fringelet carries a known final phase. The intersections (radial position) of the fringelets with the cut, thus, have a known final phase. If no fringelet intersects the cut within the interval, the mid-radius of the interval is assigned the arithmetic average of the phases of the two fringelets which "straddle" the cut. Each intersection or straddle, which assigns a known final phase to a given radius within the interval, is called a "hit". The phase shift at a hit is obtained by subtracting the initial phase at the this radius.



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Fig. 2 Shifted (final) fringes within the I'th interval, showing non-uniform decimal fringelets (dashed). Some J=4 distances shown.

The initial phase is determined by the phases of the bounding initial fringes and by interpolation using the fractional distance (at the hit radius) of the cut from the lower fringe.

The implementation of the calculations involves a bit of bookkeeping and indexing, some of which is discussed here. Phase information is recorded by sequentially numbering the final and initial fringes. They must, of course, merge to the same values in the outer most, lowest density region of the medium. The initial fringes are usually close to straight lines but are divided in the region of the cut into a small number of radial "spans" in which the fringes are accurately linear. See Fig. 3. We are primarily interested in the pairs of initial and final fringes which bound the cut at a given radius. However, due to fringes crossing the cut, these pairs change with radius. Each interval I1 determines the span, with index K (I1), and the crossing region (for final fringes), with index L (I1) of that interval. In turn, K(I1) and L(I1) determine, respectively, the bounding initial and final fringe pairs for that interval. The phase of the lower bounding fringe in an interval is determined by the fringe number: M1(K(I1)) for initial fringes and N(L(I1)) for final fringes. Each hit (intersection or straddle of a shifted fringelet with the cut), with index I, is labeled with the interval number I1(I) and fringelet number J1(I). See Fig. 2. A variable E(I) indicates whether a hit is an intersection

 $(E(I)=\emptyset)$ or is a straddle (E(I)=.5). The interpolated shifted fringe number at the hit is thus $N(L(II(I))) + (JI(I)-E(I))/1\emptyset$. The interpolated initial fringe number at the hit depends on the fraction F(I) into which the cut divides the fringe spacing at the hit radius. See Fig. 3. Here, F(I)=-WI(I)/(W2(I)-(WI(I)). Thus, the interpolated initial fringe number is MI(K(II(I)))+F(I). The phase shift (in units of pi) is thus given by twice the difference in the shifted and initial fringe number at the hit.

$$P(I)=2*(N(L(I1(I)))+(J1(I)-E(I))/10-(M1(K(I1(I)))+F(I)))$$

The final result is the hit radius R(I) and phase shift P(I), sorted for increasing radius.

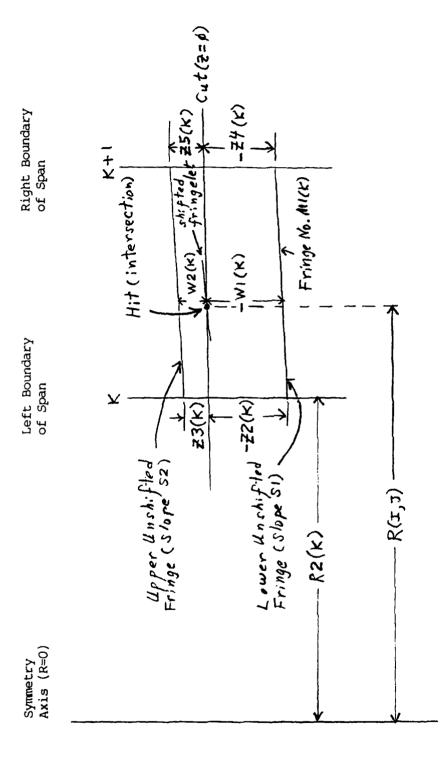


Fig. 3 Unshifted (initial) fringes within the K'th span, showing one hit (intersection of shifted fringelet and cut).

III. PROCEDURE AND EXAMPLE

A sample interferogram pair, prepared for extracting data, is shown in Fig.1. This is the superposition of two separate interferograms: The inital or pre-shot interferogram (shown dashed) and the final, shifted or data interferogram. The invidual interferograms were projected and the fringes carefully aligned to each other for reference positions and merging to the same outer fringes. This happened to be the interferogram pair from which the procedure was developed and was not the optimum pair of interferograms for accurate application of the method. It may be helpful to refer to Figs. 2 and 3, showing separately information on the initial and final interferograms.

We first draw in the cut at the desired Z-position, taking into consideration the requirement of cylindrical symmetry. We next divide the initial fringes into a small number (4, in the example) of radial regions or spans such that: (1) Initial fringe crossings only occur at 3pan boundaries and (2) the fringes are accurately linear within a span. The symmetry axis $(R=\emptyset)$ and outer radius (of fringe shifting) are taken as span boundaries. Spans are designated (K) by their left, or inner boundary. Span boundaries (vertical lines) are extended into the region above the cut and the following symbols used to aid recognition: ψ (for span boundary), k (for initial fringe crossing the cut).

Each span is labeled with the span index (K) and lower initial fringe number (M1) of fringes bounding the cut. It is also helpful to note the span boundary radii at each span boundary.

Information about the shifted fringes is indicated in the region well below the cut. First, locate all shifted fringe crossings, pass a vertical line through each crossing and indicate with a slanted dash (matheral) that it is a crossing. Label each crossing region (below the cut) with the crossing index L and lower shifted fringe number N e.g., (matheral matheral matheral). Next, draw in (short vertical lines) interval boundaries such that: (1) all fringe crossings (initial or shifted) and span boundaries are interval boundaries, and (2) the final (shifted) fringes are linear in each interval. Intervals are designated (I) by the left or inner boundary. The symmetry axis (I=1, where R=matheral) and outer radius (I=Imatheral+1, where Imatheral6 is the number of intervals) are also interval boundaries. The interval number of the shifted fringe crossings are indicated below the crossing (e.g., I=7).

We are now in a position to organize the information in tabular form, on data sheets, so that it can be input to the program. At the top of the first sheet, note the identifying (e.g., shot) number, the magnification (needed in Abel inversion) and the number of intervals ($I\emptyset$), spans ($K\emptyset$) and shifted fringe crossings ($N\emptyset$). Since lower fringe numbers (used in

calculating phase) depend directly on the span (initial) and the crossing region (shifted) while information is input for each interval, it is useful to relate each interval index to a span and crossing index. This cross-indexing is calculated by inputs from Table I. Next we record (in Table II) the lower fringe numbers.

The next step is to make detailed measurements of radial and axial distances and to organize this data into tabular form. In the shifted fringes, it is necessary to measure and record (in Tables III and IV), for each interval, the interval index I, the radial position R1(I) of the left boundary, the axial position (negative) Z1(I) of the lower fringe from the cut, the fringe slope SØ(I)=(dZ/dR)/ABS(dZ/dR), and the lower, central, and upper fringe-pair spacings D1(I), D2(I), D3(I). The distances are all measured in centimeters. The fringe slope is Ø for the cut and +1 or -1 according as Z increases or decreases with R for a fringe. CAUTION: At a fringe crossing, we can have either a $J=\emptyset$ intersection (where $Z1(I)=\emptyset$, since SØ(I)=-1) or a $J=1\emptyset$ intersection (where Z1(I)=-DZ(I), since SØ(I)=1).

The shifted fringe input is first recorded, in Table III for the outermost radius (where $I=I(\hat{p}+1)$). The shifted fringe input at all left interval boundaries (I=1 to $I(\hat{p})$ is recorded in Table IV.

The input data for the initial fringes are recorded at each span. This includes the radius R2(K) of the (left-hand) span boundary, the axial positions (negative) of the left-side Z2(K) and right-side (Z4(K) of the lower fringes and the axial positions (positive) of the left-side Z3(K) and the right-side Z5(K) of the upper fringes. The values are recorded (Table V) for the left boundaries of the individual spans.

The detailed shifted-fringe information for each interval (Table IV) is entered, before the program is run, into DATA statements near the end of the program. The data for cross-indexing (Table I), lower fringe identification (Table II), outer radius information for shifted fringes (Table III), and the intial fringe information (Table V) are entered during the running of the program, as requested by input statements.

Interferometry Data Sheet - 1 (Enter as requested by program, during run)

Shot No. 14760 Mag. M=19 $1\emptyset=21$ K $\emptyset=4$ N $\emptyset=4$

Table I. Cross-Indexing: The intervals (left interval boundaries) I2 which occur at interior fringe crossings and the intervals (left boundaries) I3 which occur at interior span boundaries are:

Crossing Index L-1	Interval Index I=I2(L-1)	Span Index K-1	Interval Index I=I3(K-1)
1	7	1	3
2	10	2	7
3	15	3	18

Table II. The lower (shifted/initial) fringe numbers vs.
(region/span) index (L/K).

Index L	Fringe # N(L)	Index K	Fringe # M1(K)
1	3	1	1
2	4	2	2
3	5	3	3
4	4	4	4

<u>Table III</u>. Shifted fringe input for the outermost radius ($I\emptyset+1$).

R1=15.3	Z1=0	SØ=-1
D1= .30	D2=.30	D3 = .30

Interferometry Data Sheet - 2 (Enter in Data Statements; 1 interval per statement)

Table IV. At the left (inner) boundary of each interval, the index I, radius R1(I), axial position of lower fringe Z1(I), fringe slope S0(I), and lower, central and upper fringe-pair spacings D1(I), D2(I), D3(I) are:

I	R1(I)	Z1(I)	SØ(I)	D1(I)	D2(I)	D3(I)
1 2	0 0.87	19 22	-1 -1	.40	.40	.35
3 4 5 6 7	1.78 2.52 3.69	30 26 23	-1 -1 -1	.40 .38 .36	.40 .38 .38	.40 .32 .34
6 7 8	5.02 6.50 7.10	25 0 08	-1 -1 -1	.36 .37 .38	.35 .32 .30	.30 .32 .32
9 10 11	8.40 9.02 9.28	14 0 02	-1 -1 -1	.38 .28 .30	.30 .30 .32	.28
12 13	9.45 9.67	07 13	-1 0	.31 .27	.33	.34
14 15 16	9.90 10.18 10.37	12 25 14	1 1 1	.24 .20 .20	.30 .25 .24	.34 .25 .33
17 18 19	10.69 10.92 11.51	10 10 13	1 0 -1	.29 .30 .32	.22 .22 .27	.32 .33 .29
20 21	12.52	17 20	-1 -1	.30	.28	.29

(Enter or requested by Program, during run)

Table V. Initial Fringe Information. The Radii and Axial Position at the Span Boundaries are:

Span Index K	Radius R2(K)	Lower Z2(K)	Fringe Z4(K)	Upper Z3(K)	Fringe Z5(K)
1	0	18	30	.12	0
2	1.78	. 0	31	.31	Ö
3	6.50	0	30	.30	Ó
4	10.92	0	29	.29	Ō

IV. Computer program with data input for the interferogram pair shown in Fig. 1.

```
10 PRINT INIFOL, A PROGRAM USING MON-UNIFORMLY-SPACED INTERFERENCE FRINGE DECI-
  MAL- INTERPOLATION. DECIMAL (INTERPOLATED) FRINGES ARE CALLED FRINGELETS.
20 PRINT "THE RADIAL VARIATION OF PHASE IS DETERMINED AT A FIXED AXIAL POSITION
  OR LINE, CALLED THE CUT.*
30 INPUT "SHOT OR IDENTIFYING NUMBER AND MAGNIFICATION": ID .MG
40 PRINT "THE SHIFTED FRINGES ARE MEASURED FOR MANY RADIAL"
                                                        INTERVALS WITH IN
50 PRINT "THE INITIAL FRINGES ARE TAKEN AS LINEAR FOR A FEW RADIAL SPANS
WITH INDEX K(I)
60 PRINT TALL SHIFTED AND INITIAL FRINGE CROSSINGS ARE TAKEN AT INTERVAL BOUN-
DARIES.ALL UNSHIFTED FRINGE CROSSINGS ARE AT SPAN BOUNDARIES."
70 INPUT "THE NUMBER ID OF RADIAL INTERVALS IS": 10
80 INPUT "THE NUMBER KO OF RADIAL SPANS IS" ; KO
90 INPUT THE NUMBER NO OF SHIFTED FRINGE CROSSINGS IST; NO
1, (61) 21, (62) 11, (62) H, (02) 6, (62) 3, (62) 20, (62) 10, (62) 1, (62) 1, (62) 1, (62) 1, (62) 1, (62) 1,
3(10), J1(50), K(30), L(30), M1(10), N(10), R1(30), R2((0), $0(30), Z1(30)
110 Dim Z2(10),Z3(10),Z4(10),Z5(10)
(11,683,51,011,68); (11,68); (11,768); (11,68); (11,68); (11,68); (11,68); (11,68); (11,68); (11,68); (11,68);
130 '---
140 -----SHIFTED FRINGE CALCULATIONS-----
150
163 '-----INCEXING TO INTERVAL AND NUMBERING------
170 PRINT "INTERVALS ARE LARELED BY THEIR INNER OR LEFT BOUNDARY"
180 PRINT THE SHIFTED FRINGE CROSSINGS ARE LOCATED AT INTERNAL BOUNDARIES 10+1
   AND AT I="
190 ----- = CROSSING INDEX L-1 FOR FOLLOWING LOOP------
203 FOR I=1 TO NO-1
210 INPUT *IZ(L-1)=*;IZ(I)
200 NEKT I
220 L=0
240 ------ I=INTERVAL INDEX FOR FOLLOWING LOOP----------
250 U1 =1
263 FOR I=1 TO I2(NO-1)
270 IF I(I2(U1) THEN 290
280 U1=U1+1
290 L(I)=U1
300 NEXT I
310 FOR I=12(NO-1) TO 10
320 L(I)=N0
330 NEXT I
340 PRINT "THE SHIFTED (LOWER) FRINGE NUMBERS APE"
350 FOR L=1 TO NO
360 INPUT "N(L)=";N(L)
370 NEXT L
380 PRINT "THE (LOWER) FRINGE-SLOPE VARIABLE SQ(I) IS (dZ/dR)/ABS(dZ/dR)"
390 '-----
400 '-----READ AND INPUT DATA AT EACH INTERVAL------
 410 PRINT "THE INTERVAL INDEX I. RADIAL (LEFT) BOUNDARY POSITION RICE), (NEG.)
    AXIAL POSITION IN(I), FRINGE-SLOPE VARIABLE 50(I) AND THE LOWER, CENTRAL AND
 UPPER FRINGE-PAIR SPACINGS D((1),D2(1),D3(1) APE READ IN FOR EACH DATA LINE.*
 420 ******ZI(I) IS THE LEFT-SIDE AXIAL POSITION OF THE LOWER SHIFTED FRINGE.FOR
    430 FOR I=: TO 10
 440 READ I RI(I).ZI(I).S0(I).D1(I).D2(I).D3(I)
 450 NEXT I
 460 INPUT "AT THE OUTER RADIUS (I-10+1) Rt,Z1,S0,D1,D2,ANG 03 ARE::R1([0+1),
       Z1(10+1),50(10+1),D1(10+1),D2(10+1),D3(10+1)
 460 Thermal Boundaries -----
 420 FOR I = 1 TO IO-1
500 G(I) = (CO(I) - D((I)))/180
 510 H(T) * (D2(I) - D1:I1)/IC
```

```
520 A(1) = (D1(1) + D2(1) 1/20
530 8(T) = (-19.6(T) + 9.H(T))/8
540 C(I) = (3*6(I) - H(I))/8
550 NEXT I
560 FOR I=1 TO 10+1
S70 X(I,0)=0
580 Z(I,0)=Z1(I)
S90 NEXT I
600 FOR I = 1 TO I0+1
610 FOR J = 1 TO 9
829 V(I,J) = 8(I) + (2*J - 1)*C(I)/3
630 X(I,J) = J \cdot (A(I) + (J-i) \cdot V(I,J)/2)
640 Z(I,J) = ZI(I) + X(I,J)
650 NEXT J
860 Z(I,10) = Z1(I) + D2(I)
670 NEXT I
680 '-----
690 '-----RIGHT-HAND INTERVAL BOUNDARY VALUES------
700 FOR I = 1 TO IO
710 FOR J = 1 TO 10
720 IF Z'(I+1) = 0 OR Z!(I+1) = -DZ(I+1) THEN 750 ELSE 730
730 XI(I,J) = X(I+I,J)
740 GOTO 790
750 IF Z1(I+1) = 0 THEN 760 ELSE 780
760 X1(I,J) = (D1(I+1)/D2(I))*X(I,J)
770 GOTO 790
788 X1(I,J) = (03(I+1)/D2(I))*X(I,J)
790 IF Z1(I+1) * 0 THEN 900 ELSE 820
800 ZS(I,J) = XI(I,J) - DI(I+1)
810 0070 853
820 IF Z1(I+1) = -02(I+1) THEN 830 ELSE 850
830 \ Z5(I,J) = X1(I,J)
840 GOTO 860
850 Z6(I,J) = Z1(I+1) + X1(I,J)
860 NEKT J
870 NEXT I
860 '----
890 '----FIND HITS (FRINGELET INTERSECTIONS WITH OR STRADDLES OF CUT)-----
900 -----RADIAL POSITION IN INTERVAL IS-----
910 FOR I - 1 TO 10
920 FOR J= 1 TO 9
930 Y(I,J) = -Z(I,J) \cdot (R1(I+1) - R1(I))/(Z6(I,J) - Z(I,J))
 940 NEXT J
950 NEXT I
 960 H - 1
970 FOR I * 1 TO IO
 980 IF Z1(I) - 0 THEN 990 ELSE 1010
 990 J - 0
 1000 6010 1183
 1010 IF Z1(I) = -02(I) THEN 1020 ELSE 1040
 1020 J - 10
 1030 GOTO 1180
 1040 J = 1
 1050 IF ABS(Z6(I,1) - Z(I,1))<.001 THEM 1070 '--FRINGELET 1 PARALLEL TO CUT--
 1060 IF Z6(I,1)>Z(I,1) AND Z6(I,1)>0 THEN 1180
 1070 FOR J = 2 TO 9
 1080 IF ABS(Z6(I,J) - Z(I,J))<.001 THEW 1110 THERMINGELET J PARALLEL TO CUT-
 1090 IF J-3 GOTO 1110
 1100 IF Y(1,J)>0 AND Y(1,J)(R1(1+1)-R1(1) THEN 1130 "--INTERSECTION TEST--
 1110 IF Z(1,J)/Z(1,J-1)<0 AND Z6(1,J)/Z6(1,J-1)<0 THEN 1260 '--STRADDLE TEST--
 1120 NEXT J
 1150 NEXT I
 1140 GOTO 1330
 1153
```

```
1170 -----INTERSECTION COUNTER FOLLOWS------
1180 H = H + 1
1190 E(H) = 0
1200 II(H) = I
1210 J1(H) = J
1220 IF J=0 THEN 1040 ELSE 1230
1230 IF J = 10 THEN 1040 ELSE 1240
1240 IF J=1 THEN 1070 ELSE 1120
1250 -----STRACOLS COUNTER FOLLOWS-----
1250 H = H + 1
1270 E(H) = .5
1280 [1(H) = I
1290 J1(H) = J
 1300 6010 1120
1310 -----CUTER INTERSECTION
1320 I = I3
1330 IF Z1(10) < Z1(10-1) THEN 1340 ELSE 1350
 1340 J = 10
1350 3070 1370
1380 J = 0
 1373 H = H + 1
 1363 E(H) = 3
 1798 TI(H) → T
1430 J1(H) = J
1410 PPINT THE NUMBER H OF HITS IST,H
 1420 DIM F HOLPKHOLRKAHOLSKHOLS(A),S2(A),W (H),WZ(A)
 1440 8(1) = 0
 1450 [1(1) = 1
 1460 E(1) = 3
 1470 IF Z1(1) = 0 THEN 1480 ELSE 1500
 1483 J:(1) = 0
 1490 5070 1640
 1508 FOR J - 1 TO 9
 1513 IF Z(1,1) = 0 THEN 1520 ELSE 1540
  1520 J1(1) = J
 1530 GOTO 1640
  1540 NEXT J
  1580 E(1) = .5
  1560 IF Z(1,1) >0 THEN 1570 ELSE 1590
  1570 J1(1) = 1
  1580 GOTO 1640
  1590 FOR J = 2 TO 10
  1600 IF Z(1,J)/Z(1,J-1)(0 THEN 1610 ELSE 1630
  1619 J1(1) = J
  1620 GCTO 1640
  1630 NEXT J
  1640 '-----
  1653 '-----FIND RADII OF FRINGELET CROSSINGS-----
  1663 FOR I = 2 TO H - I
  1670 IF Z([1([),J1([)) C) 0 THEN 1680 ELSE 1730
  1630 IF E(T) = 0 THEN 1630 ELSE 1710
  1692 \ R(I) = R(I(I(I)) - Z(I(I),J(I)) \cdot (R(I(I(I)+1) - R(I(I(I)))/(Z6(I(I)-J))) + R(I(I(I))) + R(I(I)) + R(I(
  (I)) ~ Z(I!(I),J!(I)))
  1703 6070 1743
  1710 R(I) = .5*(R1(I1(I)) + R1(I1(I) + I))
  1720 3010 1740
  1730 P(I) = R1(I1(I))
   1748 NEXT I
  1750 A(H) = R1([0+1)
1750 FOR I = 1 TO H
1770 LPRINT THITS AT H E I J R=1:1 E [/:[/[]:[]:[]:[] R([):
```

```
1780 NEXT I
1790 'STOP
1800
1810 '-----INITIAL FRINGE CALCULATIONS-----
1829
970 '-----SPAN-TO-INTERVAL INDEXING-----
1830 PRINT "THE SPAN BOUNDARIES ARE LOCATED AT I = 1,10 + 1, AND AT"
1840 ----- K -1 FOR THE FOLLOWING LOGP------
1850 FOR I = 1 TO KO-1
1860 INPUT "I3(K-1) ="; I3(I)
1870 NEXT I
1880 K - 0
1890 U2 = 1
1900 -----I = INTERVAL FOR FOLLOWING LOOP-------
1910 FOR I =1 TO I3(K0 - 1)
1920 IF IKI3(U2) THEN 1940
1930 U2 = U2 + 1
1940 K(I) = U2
1950 NEXT I
1960 FOR I = I3(K0 - 1) +1 TO I0
1970 K(I) = K0
1980 NEXT I
1990
2000 PRINT "THE LEFT-HAND SPAN BOUNDARIES ARE AT RADII" [-----RZ(1)=0-----
2010 FOR I = 1 TO KO
2020 INPUT TRO(K) =1;R2(I)
2030 NEKT I
2040 R2(K0+1) = R1(I0+1)
2060 PRINT THE INITIAL LOWER FRINGE NUMBERS ARET
2070 FOR I = 1 TO KO
2080 INPUT "MI(K) =":MI(I)
2090 NEXT I
2100 '-----
2:10 '-----FINO L,K,N,M1 AT HITS-----
2120 '-----
2130 PRINT THE LEFT-SIDE AXIAL POSITIONS (NEG.) OF THE LOWER INITIAL FRINGES
  ARE"
2140 FOR I - 1 TO KO
2150 INPUT "Z2(K) =";Z2(I)
2160 NEXT I
2178 -----
2180 PRINT "THE RIGHT-SIDE AXIAL POSITIONS (NEG.) OF THE LOMER INITIAL FRINGES
   ARE"
2190 FOR I=1 TO KO
2230 INPUT "Z4(K)=":Z4(I)
2210 NEXT I
2220 '------
2230 PRINT "THE LEFT-SIDE AXIAL POSITIONS (POS.) Z3(K) OF THE UPPER INITIAL
  FRINGES ARE"
2240 FOR I = 1 TO K0
2250 INPUT *Z3(K)=*;Z3(I)
2280 PRINT THE RIGHT-SIDE AXIAL POSITIONS (POS.) OF THE UPPER INITIAL FRINGES
  ARE"
 2290 FOR I= 1 TO KO
2300 INPUT "Z5(K)=";Z5(I)
 2310 NEXT I
    -----FIND INITIAL FRINGE FRACTION AT EACH HIT------
 FRINGES AT A HIT, WHILE ST AND S2 ARE THE FRINGE SLOPES------
 2358 F(1) + -Z2(1)/(Z2(1) - Z2(1))
```

```
2350 FOR I = 2 TO H-1
 2370 \text{ Si(I)} = (24(K(I)(I))) - 22(K(I)(I))))/(R2(K(I)(I)) + 1) - R2(K(I)(I))) \\ 2380 \text{ S2(I)} = (25(K(I)(I))) - 23(K(I)(I))))/(R2(K(I)(I)) + 1) - R2(K(I)(I))) 
2390 WI(I) = Z4(K(II(I))) - SI(I)*(R2(K(II(I)) + I) - R(I))
2400 \text{ W2(I)} = Z5(K(I1(I))) - S2(I)*(R2(K(I1(I)) +1) - R(I))
2410 F(I) = -W1(I)/(W2(I) - W1(I))
2420 NEXT I
2430 F(H) = (1 ~ S0(I0))/2
2440 FOR I =1 TO H-1
2450 'PRINT "H.St.,SZ.WI.WZ=";I;S1(I);SZ(I);W1(I);WZ(I)
2460 NEXT I
2470 'STOP
2480 -----
2490 '-----FINO THE PHASE SHIFT P(I) AT EACH HIT-------
2500 FOR I = 1 TO H-1
2510 P(I) = 2*(N(L(I1(I))) + (J1(I) - E(I))/10) - 2*(M1(K(I1(I))) + F(I))
2520 NEXT I
2530 P(H) = 0
2540 'STOP
2550 '-----
2560 -----SORT AND INDEX FOR INCREASING RADIUS-----
2570 FOR I = 1 TO H
2580 S(I) = I
2590 RR(I) = R(I)
2500 NEXT I
2510 NR - H
2620 IS - 0
2530 NR = NR - 1
2640 FOR I = 1 TO NR
2550 IF R(I) < R(I+1) GOTO 2730
2660 IS = 1
2670 RH = R(I+1)
 2680 R(I+1) = R(I)
2690 R(I) = RH
2700 SH - S(I+1)
 2710 S(I+1) = S(I)
 2720 S(I) - SH
 2730 NEXT I
 2740 IF IS = 1 60TO 2620
 2750
       -----FINAL RESULTS-------
 2770 FOR I - 1 TO H
 2780 LPRINT "H N,M) F=";S(I),N(L(I1(S(I))));H1(K(I1(S(I)))),F(S(I))
 2790 NEXT I
 2800 'STOP
 2810 FOR I - 1 TO H
 2820 LPRINT "H,E,I,J,R,P";S(I);E(S(I));I1(S(I));J1(S(I)),RR(S(I)),P(S(I))
 2830 NEXT I
 2840 STOP
 2850 '-----
 2860 '-----DATA-----DATA-----
 2870 DATA 1,0,-.19,-1,.4,.4,.35
 2880 DATA 2,.87,-.22,-1,.38,.38,.38
 2890 DATA 3,1.78,-.3,-1,.4,.4,.4
 2900 DATA 4,2.52,-.26,-1,.38,.38,.32
 2910 DATA 5,3.63,-.23,-1,.36,.38,.34
 2920 DATA 6,5.02,-.25,-1,.36,.35,.30
 2930 DATA 7, 6.50,-0.0,-1,.37,.32,.32
2940 DATA 8, 7.10,-.08,-1,.38,.30,.32
 2950 DATA 9, 8.40,-.14,-1,.38,.30,.28
  2960 DATA 10, 9.02,-0.0,-1,.28,.30,.30
 2970 DATA 11, 9.28,-.02,-1,.30,.32,.33
2980 DATA 12, 9.45,-.07,-1,.31,.33,.34
2990 DATA 13, 9.57,-.13, 0,.27,.33,.34
 3000 DATA 14, 9.90,-12, 1,24,30,34
3010 DATA 15,10,18,-25, 1,20,25,25
```

3020 DATA 16,10.37,-.14, 1,.20,.24,.33
3030 DATA 17,10.69,-.10, 1,.29,.22,.32
3040 DATA 18,10.92,-.10, 0,.30,.22,.33
3050 DATA 19,11.51,-.13,-1,.32,.27,.29
3060 DATA 20,12.52,-.17,-1,.30,.28,.29
3070 DATA 21,13.58,-.20,-1,.29,.29,.30
4000 END

V. Final results, giving hit number (H), straddle index(E), interval index (I), fringelet index (J), and radius (R) and phase (P) at each hit.

```
H,E,I,J,R,P 1
               .5 1 5
                                             3.7
H,E,I,J,R,P 2
               0 1
                     5
                              .2696167
                                             3.678824
H,E,I,J,R,P 3
               0
                  2
                              .9770586
                     6
                                             3,560872
H,E,I,J,R,P 4
               0
                  2
                     7
                              1.504242
                                             3,523936
H,E,I,J,R,P 5
                  3
                     7
               0
                              2.2538
                                             3.199322
H,E,I,J,R,P 6
               0
                  4
                     6
                              3.675732
                                             2.396723
H,E,I,J,R,P 7
                Ø
                  5
                     6
                              3.70243
                                             2.385411
H,E,I,J,R,P 8
               0
                  5
                     7
                              5.008705
                                             2.031905
H,E,I,J,R,P 9
                0
                   6
                      8
                              5.504912
                                             2.021648
H,E,I,J,R,P 10
                      9
                0
                   6
                              6.000796
                                             2.011532
H,E,I,J,R,P 11
                   7
                 0
                       0
                              €.5
H,E,I,J,R,P 12
                   7
                       2
                 0
                              6.997422
                                             2.174922
H,E,I,J,R,P 13
                Ø
                   8
                       3
                              7.452748
                                             2.164368
H,E,I,J,R,P 14
                0
                   8
                      4
                              8.123563
                                             2.065356
                   9
H,E,I,J,R,P 15
                Ø
                      5
                              8.469821
                                             2.108678
H,E,I,J,R,P 18
                   9 6
                0
                              8.53581
                                             2.256195
                   9
H,E,I,J,R,P 17_ 0
                      .7
                              8.697731
                                             2.405551
                   G
                       8
H,E,I,J,R,F 18
                0
                              8.805726
                                             2.556233
H,E,I,J,R,P 19
                    9
                       9
                 Ø
                              8.913634
                                             2.707768
H,E,I,J,R,P 20
                        0
                 0
                    10
                              9.020001
                                             2.859728
H,E,I,J,R,P 21
                 0
                    11
                        2
                              9.429931
                                             3.074239
H,E,I,J,R,P 22
                 Ø
                    12
                        3
                              9.543399
                                             3.222897
H,E,I,J,R,P 23
                 0
                    12
                        4
                              9.657842
                                             3.371112
H,E,I,J,R,P 24
                 .5
                    13
                        5
                              9.785
                                             3.413574
H,E,I,J,R,P 28
                    14
                        4
                 Ø
                              9.919374
                                             3.252772
H.E,I,J,R,P 27
                 0
                    14
                        3
                              9.996132
                                             3.01804
H,E,I,J,R,P 25
                 0
                    14
                        2
                                             2.78712
                               10.05445
H,E,I,J,R,P 25
                 0
                    14
                        1
                               10.12546
                                             2.559523
H,E,I,J,R,P 29
                Ø
                    15
                        10
                               10.13
                                             2.334842
H,E,I,J,R,P 32
                Ø
                    15
                        9
                               10.22922
                                             2.112569
H,E,I,J,R,P 31
                 Ø
                    15
                        8
                               10.28099
                                             1.889144
H,E,I,J.R,P 30
                 0
                    15
                        7
                               10.33225
                                             1.68595
H,E,I,J,R,P 34
                 Ø
                    16
                        6
                               10.42388
                                             1.42449
H,E,I,J,R,P 33
                 Ø
                    16
                        5
                               10.62143
                                             1.1351
H,E,I,J,R,P 35
                 .5
                     17
                         5
                               10.805
                                              .9520359
H,E,I,J,R,P 36
                 .5
                     18
                        5
                               11.215
                                             .765296
H,E,I,J,R,P 37
                    19
                 0
                        5
                               11.7056
                                             .6408196
H,E,I,J,R,P 38
                 Ø
                    19
                               12.46659
                                              .4937954
H,E,I,J,R,P 39
                 .5
                     20 7
                               13.05
                                              .3273974
H,E,I,J,R,P 40
                 Ø
                    21
                        7
                               13.61929
                                              .1674431
H,E,I,J,R,P 41
                 0
                    21
                        8
                               14.16355
                                              .118928
H,E,I,J,R,P 42
                 Ø
                    21
                        9
                               14.7233
                                             6.333351E-02
H,E,I,J,R,P 43
                 Ø
                        10
                               15.3
```

VI. APPENDIX

Interpolation of the non-uniformly-spaced shifted fringes is accomplished by dividing the axial space between the two fringes which bound the cut, within an interval, into ten non-uniform spaces by introducing decimal "fringelets". The lower bounding fringe is taken as the J=Ø fringelet and the upper bounding fringe is taken as the J=lØ fringelet. Refer to Fig. 2. Let D1(I), D2(I), and D3(I) denote, respectively, the axial fringe-pair spacing at the (left) interval boundary of the lower, central (bounding the cut), and upper fringe pairs. It is necessary to determine the distance D(I,J), for J=1 to 1Ø, between the J-1 and J fringelets. First require that the sum of the fringelet spacings be the central fringe-pair spacing.

$$\sum_{J=1}^{10} D(I,J) = D2(I)$$
 A1

Information about the non-uniform adjacent fringe-pair spacings is included by requiring that the lower fringelet spacing D(I,1) be one-tenth of the average fringe-pair spacing for the lower and

central fringe-pairs and that the upper fringelet spacing $D(I,1\emptyset)$ be one-tenth of the average fringe-pair spacing for the upper and central fringe pairs.

$$D(I,1)=(D1(I)+D2(I))/2\emptyset$$
 A2

$$D(I,1\emptyset) = (D2(I)+D3(I))/2\emptyset$$
 A3

In order to meet these three requirements, D(I,J) must be at least quadratic in J. It is assumed that

$$D(I,J)=A(I)+B(I)(J-1)+C(I)(J-1)^{2}$$
. A4

The coefficients A, B, and C are determined by using Eq. (A4) in Eqs. (A1-A3). It is immediately seen that A(I) is D(I,1) and is thus given by Eq. (A2). The other coefficients are evaluated, after a little algebra, as

$$B(I) = (-19*G(I)+9*H(I))/8$$
 A5

$$C(I) = (3*G(I)-H(I))/8$$
 A6

where G(I) and H(I) are defined by

$$G(I) = (D3(I) - D1(I)) / 18\emptyset$$

A7

$$H(I) = (D2(I) - D1(I)) / 3\emptyset$$
 •

8A

In calculating the intersections of the fringelets with the cut, it is necessary to know the distance X(I,J) between the lower bounding fringe and the J fringelet. This distance is the sum from J'=1 to J of D(I,J'). Evaluation of the sum shows that

$$X(I,J)=J*(A(I)+(J-1)*V(I,J)/2)$$

A9

where,
$$V(I,J) \equiv B(I) + (2J-1) * C(I)/3$$
.

A10

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